

Contact

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Met at Lake Bonneville Conference Oct 2018. Said he had map updates for Rush Valley 30x60. I assume is tiny bedrock polygons west of Oquirrh Mtns.

emailed 1/24/2019

Thickness as

~~check~~ ~~Armin + Moore~~ ~~181~~

✓ ~~Pobm~~ Stansbury Mtns ^{8000 ft.} ~~recheck~~ ^{source?}

✓ mh in Davis mtn 1490 ft (450 m) ^{seems thick}

~~✓~~ { Epc Sheeprock 1470 _{Pl. 2} or 1970' _{SK calc.}

✓ Epm 2800 Simpson (ref?)

✓ Zm Simpson incomplete > 3900' 1181 m

~~✓~~ E+I Sheeprock 1600 (490 m)

(check E regional thicknesses
& Western rx)

~~op~~ ~~Sheeprock~~

Thickness measured from RV 30x60

Greater than indicates incomplete section

Multiple values for a given location represent reasonable measurements at different locations and could be listed as a range

Kirby Estimates ~2010-2012

Unit	Location	Constraint	Thickness	
			Feet	Meters
Cl	Stansbury		1290	391
Cn	Davis	Greater than	470	142
Cn	Sheeprock		600	182
Cn	Sheeprock		700	212
Cn	Stansbury	Greater than	1080	327
Co	Davis	Greater than	470	142
Co	Sheeprock	Greater than	1150	348
Co	Stansbury	Greater than	1290	391
Cpc	Sheeprock		1970	597
Cpc	Simpson	Greater than	540	164
Cpc	Stansbury		620	188
Cpm	Davis	Greater than	2800	848
Cpm	Sheeprock		4260	1290
Ctl	Sheeprock		1570	475
Ctl	Stansbury		1170	354
Ctl	Stansbury		980	297
Cu	Davis		3100	939
Cwh	Sheeprock		340	103
Cwh	Simpson		1410	427
Cwh	Stansbury		330	100
Cwh	Stansbury		830	251
Cws	Sheeprock		550	167
Cws	Simpson		1180	357
Cws	Stansbury		340	103
Cws	Stansbury		970	294
Dsi	Vernon Hills		930	282
Dsi	Vernon Hills		670	203
Dsi	Sheeprock		1150	348
Dsi	Sheeprock		640	194
Dsi	Sheeprock		960	291
Dsi	Davis		750	227
Dsy	Sheeprock		1300	394
Dsy	Sheeprock		1480	448
Dsy	Vernon Hills		1310	397
Dsy	Sheeprock		1200	363
Dsy	Davis		590	179
IPMmc	Tintic		330	100
Mg?	Skull Valley	Greater than	600	182

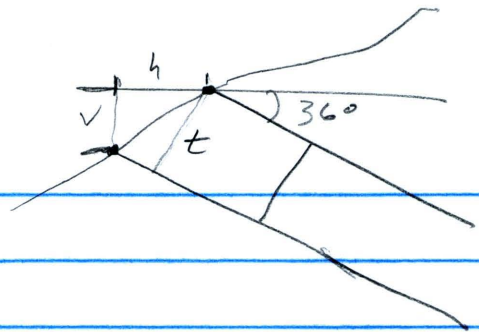
Oe	Davis		420	127
Oe	Sheeprock		1000	303
Oe	Sheeprock		420	127
Oe	Sheeprock		260	79
SOu	Davis		1420	430
SOu	Sheeprock		1310	397
SOu	Sheeprock		1070	324
SOu	Sheeprock		1690	512
Zcc	Simpson	Greater than	3850	1166
Zi	Sheeprock		600	182
Zi	Simpson	Greater than	790	239
Zm	Sheeprock		1660	503
Zm	Simpson	Greater than	3900	1181

Clark 2019 Estimates Below

Cdh	Sheeprock		765	235
Cdh	Simpson		770	235
Cww	Sheeprock		900	275
Cww	Simpson		900	275
Cpc	Simpson		390	120
Cum	Stansbury	max	6700	2045
Cum	Stansbury	min	600	185

Edh

N Sheep rocks
Red Pine



$$t = h \sin \delta + v \cos \delta$$

$$= 750 (\sin 36) + 400 (\cos 36)$$

$$v = 8000$$

$$- 7600$$

$$\underline{400 \text{ ft}}$$

$$= 441 + 324$$

$$h = 750 \text{ ft}$$

$$= 765 \text{ ft } (233 \text{ m})$$

$$765 (235 \text{ m})$$

Edw

N Sheep rocks
red pine

$$t = h \sin \delta + v \cos \delta$$

$$= (1250) (\sin 40^\circ) + (1200) (\cos 40^\circ)$$

$$\begin{array}{r} 8200 \\ - 8080 \\ \hline 120 \end{array}$$

$$= 803 + 92$$

$$= 895 \text{ ft } (273 \text{ m})$$

$$900 (275 \text{ m})$$

$$= 1000 (\sin 40) + (200) (\cos 40)$$

$$= 643 + 153$$

$$= 796 \text{ ft } (243 \text{ m})$$

Edh N Simpsons

$$t = h \sin \theta - V \cos \theta$$

$$(2100) \sin 35^\circ - (320') \cos 35^\circ$$
$$= 1205 \quad - \quad 262$$

$$900' (275 \text{ m}) = 943 \text{ ft } (288 \text{ m})$$

$$V = 3$$
$$\begin{array}{r} 5100 \\ - 5080 \\ \hline 320 \end{array}$$

$$(2100) \sin 30 - (320) (\cos 30)$$

$$1050 - 277$$

$$770 \text{ ft } (235 \text{ m}) = 773 \text{ ft } (235 \text{ m})$$

Cww N Simpsons

$$= (2700) \sin 25 - (280') \cos 25$$

$$1141 \quad - \quad 254$$

$$900' (275 \text{ m}) = 887' (270 \text{ m})$$

900

$$\begin{array}{r} 5080 \\ - 4800 \\ \hline 280 \end{array}$$

Cpc N Simpsons

$$= (1130') \sin 25 - (100') \cos 25$$

$$478 \quad - \quad 91$$

$$390' (120 \text{ m}) = 387 \text{ ft } (118 \text{ m})$$

inc.

$$\begin{array}{r} 4820 \\ - 4720 \\ \hline \end{array}$$

Sum S. Stansbury

max

$$\begin{aligned} t &= h \sin \delta + v \cos \delta \\ &= (7900') \sin 55 + (400) \cos 55 \\ &= 6471 + 229 \\ &= 6700 \text{ ft } (2043 \text{ m}) \end{aligned}$$

6700' (2045 m)

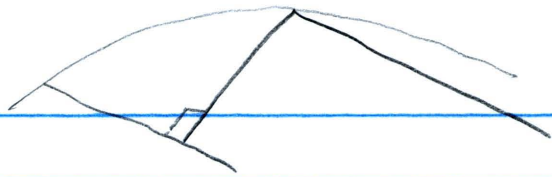
$$\begin{array}{r} v = 8000 \\ - 7600 \\ \hline 400 \end{array}$$

min

$$\begin{aligned} t &= h \sin \delta - v \cos \delta \\ &= (825) (\sin 67) - (400) (\cos 67) \\ &\quad 759 \quad - 156 \\ &= 603 \text{ ft } (184 \text{ m}) \end{aligned}$$

600' (185 m)

$$\begin{array}{r} 8000 \\ - 7600 \\ \hline \end{array}$$



Mh
Davis

$$\begin{aligned}
 t &= h \sin \delta + v \cos \delta \\
 &= (1570) \sin 55^\circ + (250) \cos 55^\circ \\
 &= 1286' + 143 \\
 &= 1429' \\
 &\rightarrow 1400' (425\text{m})
 \end{aligned}$$

$$\begin{array}{r}
 511 \\
 8722 \\
 - 6000 \\
 \hline
 250
 \end{array}$$

Epc Sheppard

$$\begin{aligned}
 t &= h \sin \delta - v \cos \delta \\
 &= (1820) \sin 40^\circ - (400) \cos 40^\circ \\
 &= 1170 - 306 \\
 &= 864' (263\text{m}) \\
 &\rightarrow 865' (265\text{m}) \\
 &\rightarrow 870' (265\text{m})
 \end{aligned}$$

$$\begin{array}{r}
 8200 \\
 7800 \\
 \hline
 400
 \end{array}$$

Epm Simpson

$$\begin{aligned}
 t &= h \sin \delta - v \cos \delta \\
 &= \left(\begin{array}{c} 10,105 \\ 10,034 \end{array} \right) \sin 20^\circ - \left(\begin{array}{c} 1000 \\ 800 \end{array} \right) \cos 20^\circ \\
 &= 3432' - 752 \\
 &= 2680' (817\text{m}) \\
 &\rightarrow 2700' (825\text{m})
 \end{aligned}$$

$$\begin{array}{r}
 6800 \\
 5800 \\
 \hline
 1000 \\
 800
 \end{array}$$

Zm Simpson

$$t = h \sin \alpha - v \cos \alpha$$

$$(4420')(\quad) - (600)(\quad)$$
$$= 1512' - 564$$

$$= 948'(\quad)$$

$$\rightarrow 950' (290 \text{ m})$$

incomplete

$$\begin{array}{r} 7200 \\ - 6600 \\ \hline 600 \end{array}$$

Zcc Simpson

$$t = h \sin \delta - v \cos \delta$$

$$(9900')(\frac{200}{20}) - (400)(20)$$

$$3386 - 376$$

$$= 3010'(\quad)$$

$$\rightarrow 3000' (915 \text{ m})$$

incomplete

$$\begin{array}{r} 7200 \\ - 7000 \\ \hline 200 \end{array}$$

Ch1 Tripp Sheepshead

$$t = h \sin \delta - v \cos \delta$$

$$(1745)(\sin 32) - (560)(\cos 32)$$

$$925 - 475$$

$$= 450' (140 \text{ m})$$

incomplete

$$\begin{array}{r} 7680 \\ - 7120 \\ \hline 560 \end{array}$$

Op Sheepshead

? Too thick

$$t = h \sin \delta + v \cos \delta$$

$$(3000)(\sin 45) + (200)(\cos 45)$$

$$= 2121 + 141$$

$$= 2262' (819 \text{ m})$$

$$\begin{array}{r} 6600 \\ - 6400 \\ \hline 200 \end{array}$$